

# A geometrically exact membrane model for isotropic foils and fabrics

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## The finite-strain-viscoelastic membrane model

The spatial deformation of a thin-walled structure  $\phi_s : \omega \times (-\frac{h}{2}, \frac{h}{2}) \to \mathbb{R}^3$  is decomposed into the motion of the (initially plane) midsurface  $m : \omega \subset \mathbb{R}^3 \to \mathbb{R}^2$  and of the director (initially) orthogonal to the midsurface,

$$\phi_s(x, y, z) = m(x, y) + z \varrho_m(x, y) R(x, y) . e_3, \qquad (1)$$

where  $R = \text{polar}(F) \in \text{SO}(3)$  is the orthogonal part of the deformation gradient F with out-of plane component  $R(x, y).e_3$ . The variable  $\rho_m \in \mathbb{R}$  accounts for a varying thickness, see [1, 2] for details.

**Basic idea:** introduce an *additional* field of independently evolving viscoelastic rotations  $\overline{R} \in SO(3)$ . These rotations  $\overline{R}$  are thought of as being physical meaningful but not exact continuum rotations R. With  $R_3 \equiv \overline{R}(x, y).e_3$  denoting the corresponding out-of plane component the dimensional reduction of a three-dimensional continuum

## Discretization of the model

We consider a fully implizit time discretized version of model (3). Let  $(m^{n-1}, \overline{R}^{n-1})$  be the given solution for the deformation of the midsurface and the rotations at time  $t_{n-1}$ . Now, compute the new solution  $(m^n, \overline{R}^n) \in \mathbb{V}$  at time  $t_n$  such that

$$\int_{\omega} h W(F^n, \overline{R}^n) \,\mathrm{d}\omega - W^{\mathrm{ext}, \mathrm{n}}(m^n) \mapsto \min.\,,\tag{7}$$

w.r.t.  $m^n$  at fixed  $\overline{R}^n$ . The current deformation gradient  $F^n = F(t_n)$  is

$$F^n = \left(\nabla m^n | \varrho_m^n \,\overline{R}_3^n\right),\tag{8}$$

and the current boundary conditions are

$$m_{|\gamma_0}^n(t_n, x, y) = g_d(t_n, x, y), \qquad x, y \in \gamma_0 \subset \partial \omega.$$
(9)

solid to a geometrically exact membrane model results in a deformation gradient of the form

$$F = (\nabla m | \varrho_m \,\overline{R}_3),\tag{2}$$

where  $\nabla m \in \mathbb{M}^{3\times 3}$  is the deformation gradient of the midsurface with  $m_x = (m_{1,x}, m_{2,x}, m_{3,x})^T$ ,  $m_y = (m_{1,y}, m_{2,y}, m_{3,y})^T$ .

**The problem:** find the deformation of the midsurface  $m : [0, T] \times \omega \mapsto \mathbb{R}^3$  and the independent local viscoelastic rotation  $\overline{R} : [0, T] \times \omega \mapsto SO(3, \mathbb{R})$  such that

$$\int_{\omega} h W(F, \overline{R}) \,\mathrm{d}\omega - \int_{\omega} \langle f_b, m \rangle \,\mathrm{d}\omega - \int_{\gamma_s} \langle f_s, m \rangle \,\mathrm{d}s \mapsto \min . \,, \tag{3}$$

w.r.t. m at fixed rotation  $\overline{R}$ . The strain energy density  $W(F, \overline{R})$  in (3) is of the form

$$W(F,\overline{R}) = \frac{\mu}{4} \|F^T\overline{R} + \overline{R}^TF - 2I\|^2 + \frac{\lambda}{8} \operatorname{tr} \left(F^T\overline{R} + \overline{R}^TF - 2I\right)^2.$$
(4)

Moreover, let  $W^{\text{ext}}(m)$  be the linear work of applied external forces with  $f_b$  being the resultant body forces and  $f_s$  the resultant surface traction and let  $g_d : \omega \mapsto \mathbb{R}^3$  denote the prescribed Dirichlet boundary conditions for the membrane,

$$W^{\text{ext}}(m) = \int_{\omega} \langle f_b, m \rangle \, \mathrm{d}\omega - \int_{\gamma_s} \langle f_s, m \rangle \, \mathrm{d}s \,,$$
$$m_{|\gamma_0}(t, x, y) = g_{\mathrm{d}}(t, x, y) \qquad x, y \in \gamma_0 \subset \partial\omega \,.$$
(5)

The field of local viscoelastic rotation follows an **evolution equation** 

$$\frac{\mathrm{d}}{\mathrm{dt}}\overline{R}(t) = \nu^{+} \cdot \mathrm{skew}(B) \cdot \overline{R}(t) \quad \text{with} \quad \nu^{+} := \frac{1}{\eta}\nu^{+}(F,\overline{R}), \quad \text{and} \ B = F\overline{R}^{T}.$$
(6)

Here  $\nu^+ \in \mathbb{R}^+$  represents a scalar valued function introducing an *artificial viscosity* and  $\eta$  plays the role of an *artificial relaxation time* (with units [sec]). The evolution equation (6) and parameter  $\nu^+$  are introduced into the model to preserve ellipticity of the force balance. Physically, one may imagine the viscoelastic rotation  $\overline{R}$  as *shadowing* the exact continuum rotation in a viscous sense.

#### Example: rectangular sheet

A hard sheet is loaded by dead load and subjected to in-plane displacement of one side. The figures show the initial and the deformed state after different time periods of relaxation:

The evolution equation for the rotations is mapped by a local exponential update. This implies that  $\overline{R}^n = \overline{R}^n (\nabla m^n)$  solves the following highly nonlinear problem

$$\overline{R}^{n} = \exp\left(\Delta t \,\nu_{n}^{+} \operatorname{skew}\left(F^{n}\overline{R}^{n,T}\right)\right) \cdot \overline{R}^{n-1} \quad \text{with } \nu_{n}^{+} = \frac{1}{\eta} \left(1 + \|\operatorname{skew} F^{n}\overline{R}^{n,T}\|\right)^{2}.$$
(10)

By the properties of logarithmic and exponential mapping it can be shown that (10) converges to (6) for the limit  $\Delta t \rightarrow 0$ , see [1].

The **finite element discretization** of problem (7) considers discrete subspaces  $\mathbb{V}_h$  of the continuous solution spaces  $\mathbb{V}$  for the membrane's deformation. We employ

$$\mathbb{V}_{h} = \mathcal{P}_{1}^{o}(\mathcal{T})^{3} \times \mathcal{P}_{0}(\mathcal{T})^{3 \times 3}, \qquad (11)$$

where  $\mathcal{P}_k(\mathcal{T})$  denotes the linear space of  $\mathcal{T}$ -piecewise polynomials of degree  $\leq k$ , and,  $\mathcal{P}^{o}_k(\mathcal{T})$  are the continuous discrete functions in  $\mathcal{P}_k(\mathcal{T})$  with homogeneous boundary values. Thus, the **discrete problem** reads: find the deformation of the midsurface of the membrane and the independent local viscoelastic rotation  $(m_h, \overline{R}_h) : [0, T] \times \mathbb{V}_h$ such that,

$$\int_{\omega} h W(F(m_{\rm h}), \overline{R}_{\rm h}) \,\mathrm{d}\omega - W^{\rm ext}(m_{\rm h}, \overline{R}_{\rm h3}) \mapsto \min . \,, \tag{12}$$

w.r.t.  $m_{\rm h}$  at fixed rotation  $\overline{R}_{\rm h}$  such that  $R_h$  satisfies (10).

#### Example: wrinkling of a thin foil

We apply our model to the problem of a  $2 \times 2m$  elastic foil under pressure load. The foil is 1mm thick, lays on a square obstacle (like a cloths on a table) and only the unsupported part of it can deform. A pressure of  $p_0 = 0.75$  MPa acts from above.









- [1] K. Weinberg and P. Neff: A geometrically exact thin membrane model investigation of large deformations and wrinkling, IJNME, to appear.
- [2] P. Neff: A geometrically exact viscoplastic membrane-shell with viscoelastic transverse shear resistance avoiding degeneracy in the thin-shell limit. Part I: The viscoelastic membrane-plate., ZAMP, 56 (2005), 148–182.