

Isogeometric analysis and thermomechanical contact

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Introduction

Thermomechanical systems [1]

- Nonlinear thermoelastic material models
 - Thermodynamically consistent formulation
 - Energy-momentum consistent integration schemes
- Thermomechanical contact and isogeometric analysis [2]
- Isogeometrical discretisation of bodies in contact
 - Transient isogeometric thermomechanical contact and impact problems
 - Application of Mortar concepts

First law of thermodynamics

- Lagrangian formulation of the first law

$$\dot{T} + \dot{E} = P^{\text{ext}} + Q$$

- Legendre transformation

$$E = \int_{\mathcal{B}_0} e(\mathbf{C}, \eta) dV = \int_{\mathcal{B}_0} \Psi(\mathbf{C}, \Theta) + \Theta \eta dV$$

- Energy balance equation

$$\underbrace{\int_{\mathcal{B}_0} \dot{\varphi} \cdot \dot{\pi} dV}_{T} + \underbrace{\int_{\mathcal{B}_0} \frac{1}{2} \mathbf{S} : \dot{\mathbf{C}} + \Theta \dot{\eta} dV}_{E} = \underbrace{\int_{\partial \mathcal{B}_0} \dot{\varphi} \cdot \mathbf{T} dA}_{P^{\text{ext}}} + \underbrace{\int_{\partial \mathcal{B}_0} \mathbf{Q} \cdot \mathbf{N} dA}_{Q}$$

- Time dependent deformation field

$$\boldsymbol{\varphi}(\mathbf{X}, t) : \mathcal{B}_0 \times \mathcal{I} \rightarrow \mathbb{R}^n$$

- Time dependent absolute temperature field

$$\theta(\mathbf{X}, t) : \mathcal{B}_0 \times \mathcal{I} \rightarrow \mathbb{R}$$

- Virtual work of the multi-field system

$$\begin{aligned} \int_{\mathcal{B}_0} \delta \varphi \cdot \dot{\pi} + \frac{1}{2} \mathbf{S} : \delta \mathbf{C} dV &= \int_{\partial \mathcal{B}_0^T} \delta \varphi \cdot \bar{\mathbf{T}} dA + \int_{\mathcal{B}_0} \delta \varphi \cdot \bar{\mathbf{B}} dV \\ \int_{\mathcal{B}_0} \delta \theta \dot{\eta} - \mathbf{Q} \cdot \text{Grad}(\delta \theta) dV &= \int_{\partial \mathcal{B}_0^Q} \delta \theta \bar{\mathbf{Q}} \cdot \mathbf{N} dA + \int_{\mathcal{B}_0} \delta \theta \bar{\mathbf{R}} dV \end{aligned}$$

- Constitutive laws

$$\mathbf{S} = 2 \frac{\partial \Psi}{\partial \mathbf{C}}, \quad \eta = -\frac{\partial \Psi}{\partial \theta}, \quad \mathbf{Q} = -\hat{\mathbf{K}}(\mathbf{C}, \theta) \nabla_{\mathbf{X}}(\theta)$$

Interface conditions

- Virtual work of the contact contributions

$$\begin{aligned} G_{\varphi}^c &= \int_{\partial \mathcal{B}_0^{(1),c}} t_N \delta g_N + \mathbf{t}_T \cdot (\delta \mathbf{g}_T^e + \delta \mathbf{g}_T^s) dA \\ G_{\theta}^c &= \int_{\partial \mathcal{B}_0^{(1),c}} \delta \theta^{(1)} Q_c^{(1)} + \delta \theta^{(2)} Q_c^{(2)} dA \end{aligned}$$

- Normal contact

$$g_N \leq 0, \quad t_N \geq 0, \quad t_N g_N = 0$$

- Tangential contact

$$\hat{\phi}_c := \|\mathbf{t}_T\| - \mu |t_N| \leq 0, \quad \dot{\zeta} \geq 0, \quad \hat{\phi}_c \dot{\zeta} = 0, \quad \dot{\mathbf{g}}_T^s = \dot{\zeta} \frac{\mathbf{t}_T}{\|\mathbf{t}_T\|}$$

- Thermal contact

$$Q_c^{(1)} = \gamma^{(1)} \mathbf{t}_T \cdot \dot{\mathbf{g}}_T^s - k_{\theta} |t_N| \vartheta_c, \quad Q_c^{(2)} = \gamma^{(2)} \mathbf{t}_T \cdot \dot{\mathbf{g}}_T^s + k_{\theta} |t_N| \vartheta_c$$

- Local entropy production rate

$$\dot{\eta}_c = \frac{Q_c^{(1)}}{\theta_c^{(1)}} + \frac{Q_c^{(2)}}{\theta_c^{(2)}} \geq 0$$

Mortar method

- Lagrange multiplier field

$$\mathcal{M}^h = \{\delta \mathbf{t}^{(1),h} \in \mathcal{L}^2(\partial \mathcal{B}_0^{(1),c} \cap \partial \mathcal{B}_0^{(2),c})\}$$

- Discrete contact contributions

$$\begin{aligned} G_{\varphi}^{c,h} &= \lambda_{N,A} \mathbf{n} \cdot \left[n^{AB} \delta \mathbf{q}_B^{(1)} - n^{AC} \delta \mathbf{q}_C^{(2)} \right] \\ &\quad + \lambda_{T,A} \cdot (\mathbf{I} - \mathbf{n} \otimes \mathbf{n}) \left[n^{AB} \delta \mathbf{q}_B^{(1)} - n^{AC} \delta \mathbf{q}_C^{(2)} \right] \\ G_{\theta}^{c,h} &= -\delta \Theta_A^{(1)} \left\{ \gamma_1 \lambda_{T,B} \cdot (\mathbf{I} - \mathbf{n} \otimes \mathbf{n}) \left[m^{ABC} \dot{\mathbf{q}}_C^{(1),s} - m^{ABD} \dot{\mathbf{q}}_D^{(2),s} \right] \right. \\ &\quad \left. - k_{\theta} |\lambda_{N,B}| \left[m^{ABC} \Theta_C^{(1)} - m^{ABD} \Theta_D^{(2)} \right] \right\} \\ &- \delta \Theta_A^{(2)} \left\{ \gamma_2 \lambda_{T,B} \cdot (\mathbf{I} - \mathbf{n} \otimes \mathbf{n}) \left[\bar{m}^{ABC} \dot{\mathbf{q}}_C^{(1),s} - \bar{m}^{ABD} \dot{\mathbf{q}}_D^{(2),s} \right] \right. \\ &\quad \left. + k_{\theta} |\lambda_{N,B}| \left[\bar{m}^{ABC} \Theta_C^{(1)} - \bar{m}^{ABD} \Theta_D^{(2)} \right] \right\} \end{aligned}$$

- Triple Mortar integrals

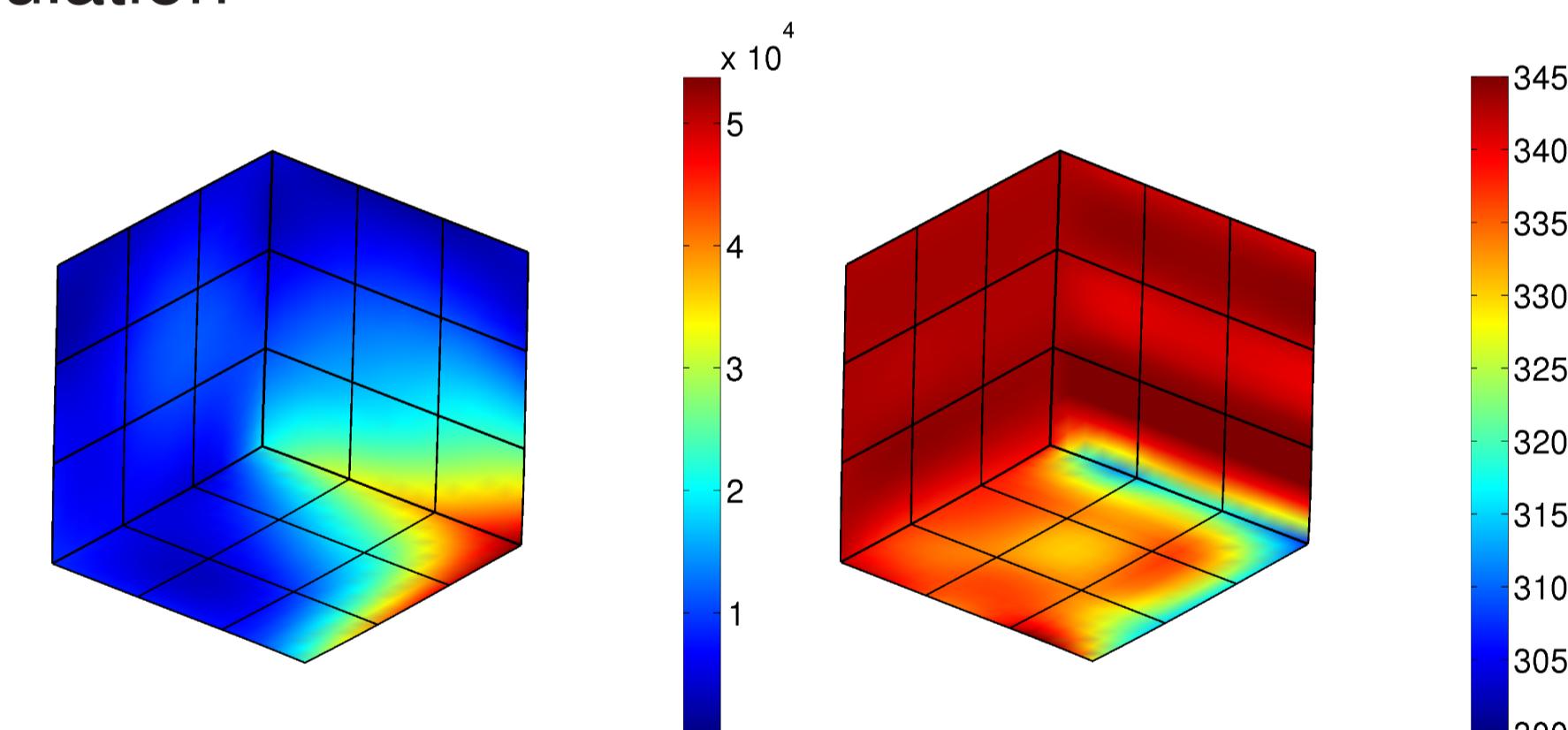
$$\begin{aligned} m^{ABC} &= \int_{\partial \mathcal{B}_0^{(1),c}} R^A(\xi^{(1)}) N^B(\xi^{(1)}) R^C(\xi^{(1)}) dA \\ m^{ABD} &= \int_{\partial \mathcal{B}_0^{(1),c}} R^A(\xi^{(1)}) N^B(\xi^{(1)}) R^D(\xi^{(2)}) dA \end{aligned}$$

Numerical example

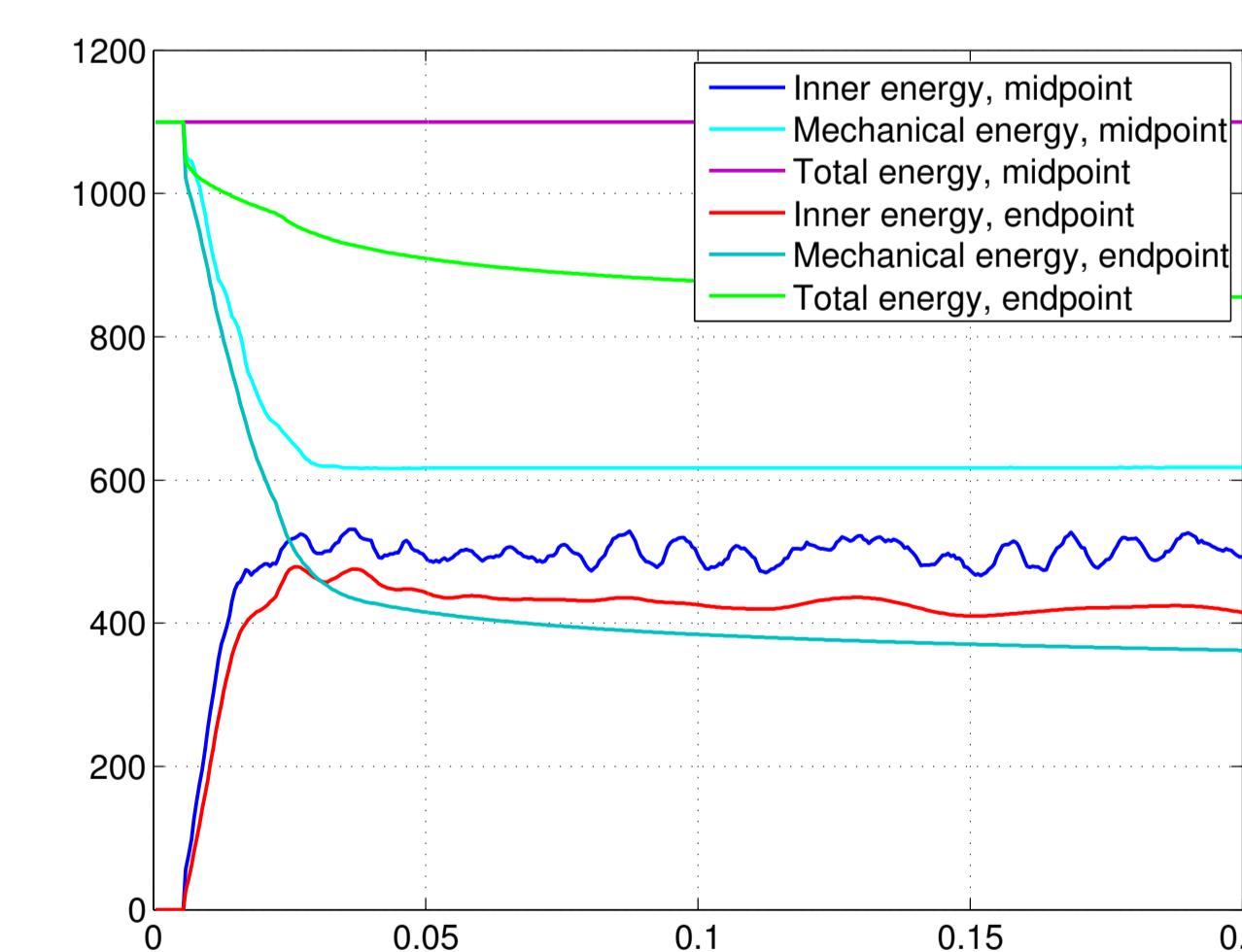
Non-linear and fully coupled Ogden material model

$$\begin{aligned} \Psi(\lambda_1, \lambda_2, \lambda_3, \theta) = & \sum_{A=1}^3 \sum_{p=1}^3 \frac{\mu_p(\theta_0) \frac{\theta}{\theta_0}}{\alpha_p} \left(\tilde{\lambda}_A^{\alpha_p} - 1 \right) + \kappa(\theta_0) \frac{\theta}{\theta_0} \beta^{-2} (\beta \ln(J) + J^{-\beta} - 1) \\ & - 3\alpha_0 \kappa(\theta_0) \gamma^{-1} (J^\gamma - 1) (\theta - \theta_0) + c_0 (\theta - \theta_0 - \theta \ln(\theta/\theta_0)) \end{aligned}$$

Impact simulation



Von Mises stresses (left) and temperature (right) distribution.



Different energies for midpoint and endpoint rule.

References

- C. Hesch and P. Betsch.
Energy-momentum consistent algorithms for dynamic thermomechanical problems
- Application to mortar domain decomposition problems.
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