

Multidimensional coupling: A variationally consistent approach to fiber-reinforced materials

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Introduction

- novel 1D fiber to 3D matrix coupling (beam/matrix)
- overlapping domain decomposition
- forces and moments of the beam are transferred
- static condensation procedure removes beam balance & coupling constraints in the discrete setting

Solid mechanics

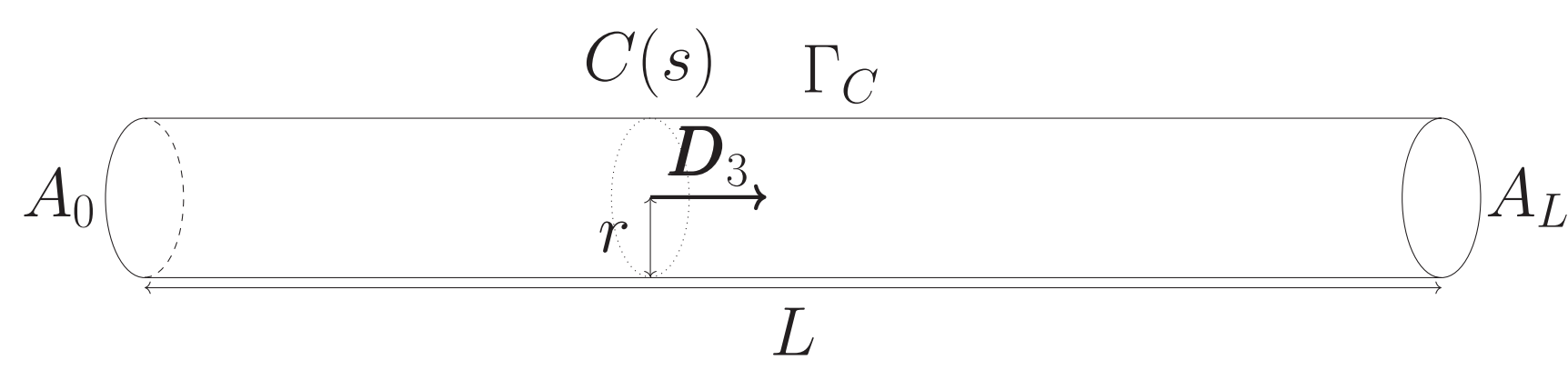
- strain energy function:

$$\Psi(\mathbf{F}) := \Psi(\mathbf{F}, \text{cof } \mathbf{F}, \det \mathbf{F})$$

- virtual work:

$$\delta \Pi^{int} + \delta \Pi^{ext} = \int_{\Omega_0} \mathbf{P} : \nabla \delta \boldsymbol{\varphi} \, dV - \int_{\Omega_0} \mathbf{B}_{ext} \cdot \delta \boldsymbol{\varphi} \, dV - \int_{\Gamma^\sigma} \mathbf{T}_{ext} \cdot \delta \boldsymbol{\varphi} \, dA$$

Continuum degenerated beam formulation



- kinematical ansatz:

$$\tilde{\mathbf{x}}(\theta^\alpha, s) = \tilde{\boldsymbol{\varphi}}(s) + \theta^\alpha \mathbf{d}_\alpha(s), \quad \tilde{\mathbf{X}}(\theta^\alpha, s) = \tilde{\boldsymbol{\varphi}}_0(s) + \theta^\alpha \mathbf{D}_\alpha(s)$$

- deformation gradient:

$$\tilde{\mathbf{F}} = \tilde{\mathbf{R}} (\boldsymbol{\Gamma} \otimes \mathbf{D}_3 + [\mathbf{K}]_\times \theta^\alpha \mathbf{D}_\alpha \otimes \mathbf{D}_3 + \mathbf{I}),$$

- axial shear & torsional-bending strain:

$$\boldsymbol{\Gamma} = \tilde{\mathbf{R}}^T \tilde{\boldsymbol{\varphi}}' - \mathbf{D}_3, \quad [\mathbf{K}]_\times = \tilde{\mathbf{R}}^T \tilde{\mathbf{R}}'$$

- strain energy function:

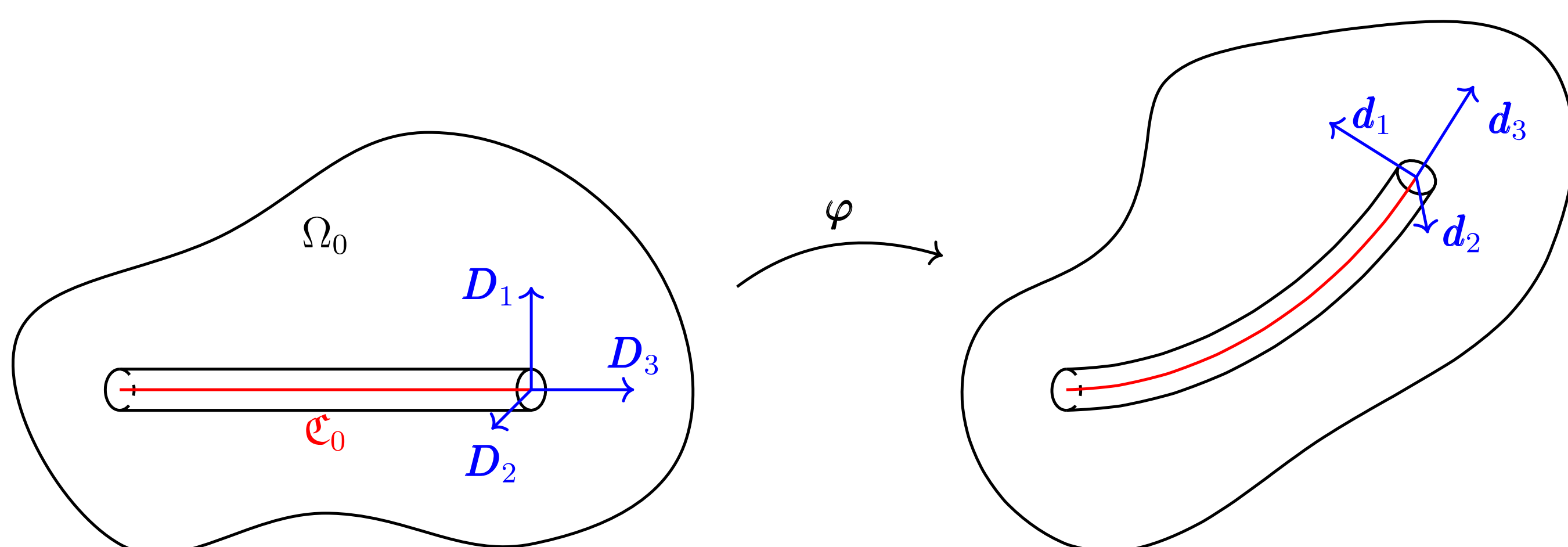
$$\tilde{\Psi} := \tilde{\Psi}(\boldsymbol{\Gamma}, \mathbf{K})$$

- virtual work:

$$\delta \tilde{\Pi}^{int} = \int_{\mathcal{C}_0} (\tilde{\mathbf{R}} \tilde{\mathbf{N}}) \cdot \delta \tilde{\boldsymbol{\varphi}}' - (\tilde{\boldsymbol{\varphi}}' \times \tilde{\mathbf{R}} \tilde{\mathbf{N}}) \cdot \delta \boldsymbol{\phi} + (\tilde{\mathbf{R}} \tilde{\mathbf{M}}) \cdot \delta \boldsymbol{\phi}' \, ds,$$

$$\delta \tilde{\Pi}^{ext} = - \int_{\mathcal{C}_0} (\tilde{\mathbf{n}} \cdot \delta \tilde{\boldsymbol{\varphi}} + \tilde{\mathbf{m}} \cdot \delta \boldsymbol{\phi}) \, ds - \llbracket \mathbf{n}_{ext}^e \cdot \delta \tilde{\boldsymbol{\varphi}} + \mathbf{m}_{ext}^e \cdot \delta \boldsymbol{\phi} \rrbracket_0^L$$

Multidimensional coupling model



- interface load:

$$\boldsymbol{\mu}(\theta, s) = \bar{\boldsymbol{\mu}}(s) + \boldsymbol{\Sigma}(s) \mathbf{N}(\theta)$$

with

$$\bar{\boldsymbol{\mu}}(s) = \frac{1}{2\pi} \int_0^{2\pi} \boldsymbol{\mu}(\theta, s) \, d\theta, \quad \bar{\boldsymbol{\mu}}_e := \frac{1}{|A|} \int_{A_e} \boldsymbol{\mu} \, dA$$

- work of coupling forces:

$$\Pi_\Gamma = \int_{\partial \tilde{\Omega}_0} \boldsymbol{\mu} \cdot (\boldsymbol{\varphi} - \tilde{\mathbf{x}}) \, dA = \Pi_C + \Pi_A$$

- virtual work:

$$\begin{aligned} \delta \Pi_C &= \int_{\mathcal{C}_0} [\delta \bar{\boldsymbol{\mu}} \cdot (\boldsymbol{\varphi}_c - \tilde{\boldsymbol{\varphi}}) + \bar{\boldsymbol{\mu}} \cdot (\delta \boldsymbol{\varphi} - \delta \tilde{\boldsymbol{\varphi}})] |C| \, ds \\ &\quad + \int_{\mathcal{C}_0} \left[\boldsymbol{\Sigma} : (\delta \mathbf{F}_c - [\delta \boldsymbol{\phi}]_\times \tilde{\mathbf{R}}) + \delta \boldsymbol{\Sigma} : (\mathbf{F}_c - \tilde{\mathbf{R}}) \right] |A| \, ds, \\ \delta \Pi_A &= \llbracket \delta \bar{\boldsymbol{\mu}}_e \cdot (\boldsymbol{\varphi}_e - \tilde{\boldsymbol{\varphi}}) |A_e| + \bar{\boldsymbol{\mu}}_e \cdot (\delta \boldsymbol{\varphi}_e - \delta \tilde{\boldsymbol{\varphi}}) |A_e| \rrbracket_0^L \end{aligned}$$

Beam/matrix system

- total system:

$$\delta \Pi^{int} + \delta \Pi^{ext} + \delta \tilde{\Pi}^{int} + \delta \tilde{\Pi}^{ext} + \delta \Pi_C + \delta \Pi_A = 0$$

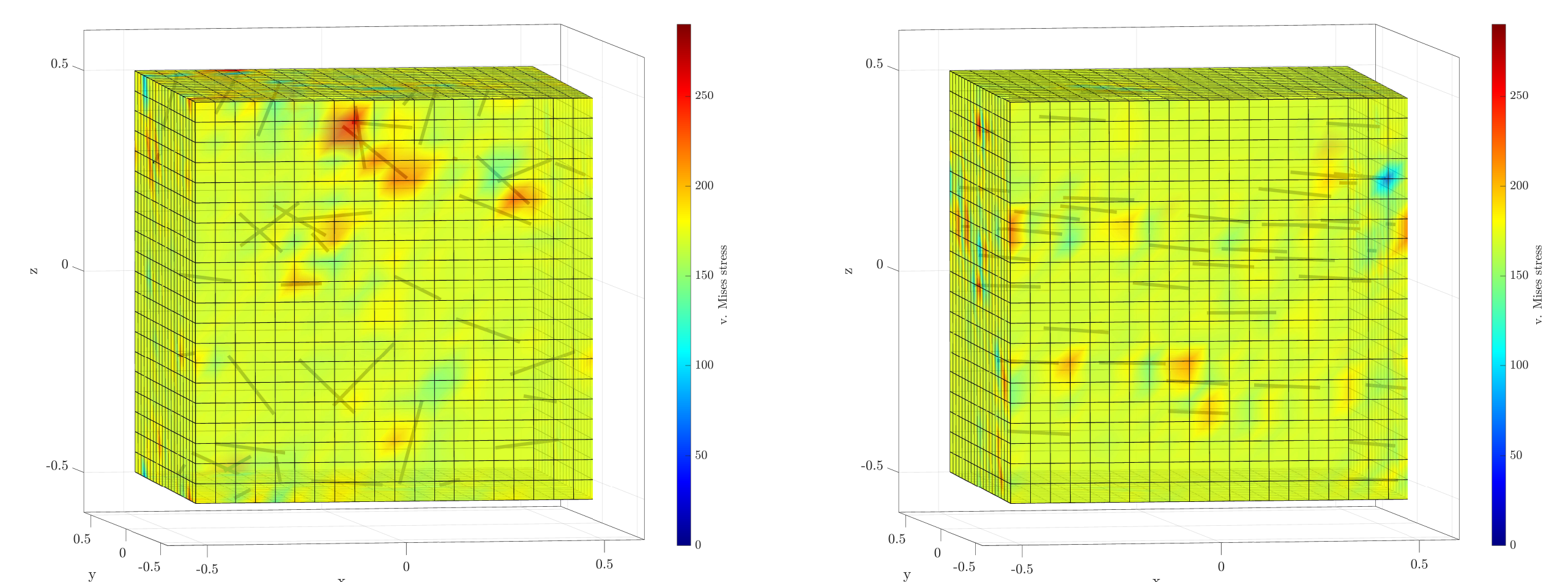
- condensed system - 2nd gradient model:

$$\begin{aligned} 0 &= \int_{\Omega_0} (\mathbf{P} : \nabla \delta \boldsymbol{\varphi} - \mathbf{B}_{ext} \cdot \delta \boldsymbol{\varphi}) \, dV - \int_{\Gamma^\sigma} \mathbf{T}_{ext} \cdot \delta \boldsymbol{\varphi} \, dA \\ &\quad + \int_{\mathcal{C}_0} \left(\mathfrak{P} : \nabla^2 \delta \boldsymbol{\varphi} + (\mathbf{P}^{ges} + \mathbf{F} [\tilde{\boldsymbol{\mu}}_n]_s |A|) : \nabla \delta \boldsymbol{\varphi} - \tilde{\mathbf{n}} \cdot \delta \boldsymbol{\varphi} \right) \, ds \\ &\quad - \left[\mathbf{n}_{ext}^e \cdot \delta \boldsymbol{\varphi} + \frac{1}{2} (\mathcal{P}_\alpha \mathbf{m}_{ext}^e \otimes \mathbf{D}_\alpha) : \nabla \delta \boldsymbol{\varphi} \right] \Big|_0^L, \\ 0 &= \int_{\mathcal{C}_0} \delta \mathbf{g} \cdot \left[\tilde{\mathbf{R}} \frac{\partial \tilde{\Psi}(\boldsymbol{\Gamma}, \mathbf{K})}{\partial \boldsymbol{\Gamma}} - \mathbf{n} \right] \, ds + \int_{\mathcal{C}_0} \delta \mathbf{t} \cdot \left[\tilde{\mathbf{R}} \frac{\partial \tilde{\Psi}(\boldsymbol{\Gamma}, \mathbf{K})}{\partial \mathbf{K}} - \mathbf{m} \right] \, ds, \\ 0 &= \int_{\mathcal{C}_0} \delta \bar{\boldsymbol{\mu}} \cdot (\boldsymbol{\varphi} - \tilde{\boldsymbol{\varphi}}) |C| \, ds + \int_{\mathcal{C}_0} \mathcal{P}_\alpha^T \mathbf{F} \mathbf{D}_\alpha \cdot \delta \tilde{\boldsymbol{\mu}}_\tau |A| \, ds \\ &\quad + \int_{\mathcal{C}_0} (\mathbf{F}^T \mathbf{F} - \mathbf{I}) : [\delta \tilde{\boldsymbol{\mu}}_n]_s |A| \, ds \end{aligned}$$

with boundary conditions $\boldsymbol{\varphi}|_{\Gamma^\varphi} = \boldsymbol{\varphi}_\Gamma$ and $\delta \boldsymbol{\varphi}|_{\Gamma^\varphi} = 0$.

Application of multiple beams

- representative volume element (RVE) for fiber reinforced plastics
- matrix - Mooney-Rivlin material, beam - Saint-Venant-Kirchhoff material
- v. Mises stress distribution



References:

- [1] Ustim Khristenko, Stefan Schuß, Melanie Krüger, Felix Schmidt, Barbara Wohlmuth and Christian Hesch. Multidimensional coupling: A variationally consistent approach to fiber-reinforced materials, Comput. Methods Appl. Mech. Engrg. 382 (2021) 113869